

# The Glass Transition Temperature of Water: A Simulation Study

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We report a computer simulation study of the glass transition for water. To mimic the difference between standard and hyperquenched glass, we generate glassy configurations with different cooling rates and calculate the  $T$  dependence of the specific heat on heating. The absence of crystallization phenomena allows us, for properly annealed samples, to detect in the specific heat the simultaneous presence of a weak pre-peak (“shadow transition”), and an intense glass transition peak at higher temperature. We discuss the implications for the currently debated value of the glass transition temperature of water. We also compare our simulation results with the Tool-Narayanaswamy-Moynihan phenomenological model.

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Much recent research has focused on the properties of glassy water, the most common form of water in the universe, which can exist in more than one distinct amorphous form[1, 2, 3]. The conversion between different glass structures, the different routes producing glass structures, and the relation between the liquid and the glass phases are under active debate.

A particularly relevant aspect of this debate concerns the identification of the glass transition temperature  $T_g$  at ambient pressure and the magnitude of the associated jump of the specific heat, an issue which has relevance also for determining the fragility of water. Extrapolation of  $T_g$  in binary aqueous solutions, in the limit of vanishing solute concentration, provides the estimate  $T_g \approx 136$  K [4]. Early differential scanning calorimetry (DSC) studies report conflicting results. Some experiments detect the glass transition [5] but others do not [6]. An exothermal peak in the specific heat of properly-annealed hyperquenched water supports the estimate  $T_g \approx 136$  K[7], with a specific heat jump of  $1.6 - 1.9$  J/mol/K. This  $T_g$  value[8, 9] has been recently debated [10, 11, 12]. It has been suggested[12] that the small peak measured in Ref. [7] is a pre-peak typical of annealed hyperquenched samples preceding the true glass transition located at  $T_g \approx 165$  K. Assigning  $T_g \approx 165$  K would explain many of the puzzles related to the glass transition in water [9, 10, 12]. Unfortunately, the  $T_g \approx 165$  K proposal can not be experimentally tested due to the homogeneous nucleation of the crystal phase at  $T_x \approx 150$  K.

Here we report a numerical study of the temperature dependence of the specific heat across the glass-to-liquid transition for the extended simple point charge (SPC/E) model for water. We analyze the effects both of the cooling rate and of annealing (“aging”) before heating the glass, since both effects are important for determining  $T_g$  [13, 14], and both effects have been studied extensively in many materials[15, 16]. Numerical studies are partic-

ularly suited since crystallization does not take place on the time scale probed in simulations. With an appropriate choice of the heating and cooling rates to mimic the experimental conditions, we show that both the shadow and the glass transition peaks can be resolved in the same heating scan. Finally, we compare the simulation results with the Tool-Narayanaswamy-Moynihan (TNM) phenomenological model [15, 17, 18].

We perform NVT molecular dynamics (MD) simulations for a system of  $N = 216$  molecules, with periodic boundary conditions. Interactions are cut off at a distance of  $r = 2.5\sigma$ , where  $\sigma$  is the length parameter defined in the SPC/E potential, and the reaction field method is implemented to account for the long range interactions. We average quantities over 32 independent trajectories at fixed density  $\rho = 1$  g/cm<sup>3</sup>. During cooling or heating,  $T$  is continuously changed by  $\delta T = q\delta t$ , where  $q$  is the cooling/heating rate, and  $\delta t = 1$  fs is the elementary time step. We perform: (i) cooling scans at constant cooling rate down to  $T = 0$  K, starting from equilibrium liquid configurations at  $T = 300$  K, (ii) heating scans at constant heating rate, starting from  $T = 0$  K glass configurations, (iii) aging at constant  $T_{age} = 100$  K, where significant aging effects are observed. We study two cooling rates  $q_c = -3 \times 10^{10}$  K/s and  $q_c = -10^{13}$  K/s, to mimic respectively the standard and hyperquenched cooling rates, and one heating rate  $q_h = +3 \times 10^{10}$  K/s. Slow experimental scan rates are typically  $\approx 0.3$  K/s, while the slowest simulation scan rate compatible with present computational facilities is  $10^7$  times faster ( $\approx 3 \times 10^{10}$  K/s). Hence, the temperature at which the system will lose equilibrium on cooling will be significantly higher in simulations than in experiment. Still, the key fact that the structural relaxation time becomes longer than the experimental (or simulation) time is the same for experiments and simulations. Therefore, as we will show below, while the  $T_g$  estimates

differ, the  $T$ -dependence and the phenomenology do not depend significantly on the scan rate. In hyperquench experiments, a cooling rate  $10^4$  times faster than the slow or ‘standard’ rate is usually achieved, while in the present simulations the faster quench rate is approximately 300 times faster than the slower quench rate.

Figure 1 shows the specific heat  $C_V(T)$  calculated by differentiating the temperature dependence of the total energy of the system on heating at the rate  $q_h = +3 \times 10^{10}$  K/s. The glass configurations are obtained by cooling equilibrium  $T = 300$  K liquid configurations at the ‘standard’ cooling rate  $q_c = -3 \times 10^{10}$  K/s. Following the usual experimental protocol, we estimate  $T_g$  from the intersection of the two dashed lines in Fig.1. The resulting value,  $T_g = 188$  K, is slightly below the lowest  $T$  at which equilibrium simulations can be performed for SPC/E[19, 20]. The  $C_V(T)$  rise of  $\approx 55$  J/mol/K, is more than an order of magnitude larger than the experimentally measured rise of  $\approx 1.6 - 1.9$  J/mol/K[13]. For  $T \gtrsim 240$  K,  $C_V(T)$  coincides with equilibrium data for the SPC/E potential[21]. Indeed, the equilibrium relaxation time of the system for  $T \gtrsim 240$  K is  $\lesssim 20$  ps, smaller than the characteristic scan time  $1$  K/ $q_h \approx 30$  ps.

We next compare in Figs. 2(a) and 2(b) the behavior of  $C_V(T)$  on heating two different glasses, the ‘standard glass’ obtained with the cooling rate  $q_c = -3 \times 10^{10}$  K/s, and the ‘hyperquenched glass’ obtained with the faster rate  $q_c = -10^{13}$  K/s. For the hyperquenched glass,  $C_V(T)$  develops a valley for  $T < T_g$ , in agreement with DSC heating scan experiments[12, 22, 23, 24] (indeed, Fig.2(a) is remarkably similar to Fig. 1 of Ref.[23]). The presence of a valley can be related to the descent of the system on the potential energy landscape upon heating with a rate slower than the cooling rate[29]. Figs. 2(a) and 2(b) show  $C_V(T)$  for the heating scan of the hyperquenched glass which has been annealed at  $T_{\text{age}} = 100$  K, for different aging times  $0 < t_{\text{age}} \leq 20$  ns. This annealing procedure is intended to mimic the experimental annealing procedure[25]. Note that aging reduces the valley in  $C_V(T)$ , and that as  $t_{\text{age}}$  increases,  $C_V(T)$  evolves towards the standard glass value (Fig. 1). Inspection of the curves for large  $t_{\text{age}}$  (Fig.2(c)) shows that a small pre-peak appears at  $T \approx 113$  K. If the standard protocol (Fig. 1) for the identification of the glass transition in the specific heat is applied, a  $T_g$  of  $\approx 75$  K is derived (Fig.2(c)). The amplitude of the peak in  $C_V(T)$  is of the order of  $1 - 2.5$  J/mol/K, and is reminiscent of the experimental value obtained in DSC measurements of hyperquenched water after annealing. In the present case, in which crystallization does not interfere with the heating scan, there is no ambiguity in associating this peak with a precursor of the true glass transition which takes place at a much higher  $T$ . To prove that the weak  $C_V$  pre-peak is outside the noise level, we show in Fig. 3 the  $T$ -dependence of the energy, where a clear maximum can be observed.

Results presented in Figs. 2 and 3 are consistent with recent anneal-and-scan experiments [12] on hyperquenched inorganic glass which does not crystallize on

heating. Our simulations thus suggest that the measured specific heat peak (Ref. [11]) which has been used to identify  $T_g$  is a pre-peak associated with the use of a hyperquenched sample combined with the annealing procedure.

Next, we discuss the possibility of modeling the simulation results using the TNM approach[15, 22, 25], which is able to model the experimental heating scan of the specific heat for glasses generated with standard cooling rates (although it fails when applied to hyperquenched glasses[23]). The TNM model assumes the response function of the system can be represented by a stretched exponential function with stretching parameter  $\beta$ . It also assumes that the relaxation time  $\tau$  depends not only on the bath temperature  $T$  but also on a fictive temperature  $T_f$  which accounts for the out-of-equilibrium condition. Narayanaswamy proposed that  $\tau$  is related to  $T_f$  by

$$\tau(T, T_f) = A \exp \left[ \frac{x \Delta h^*}{RT} + \frac{(1-x) \Delta h^*}{RT_f} \right] \quad (1)$$

where  $0 \leq x \leq 1$ ,  $\Delta h^*$  and  $A$  are constants and  $R$  is the ideal gas constant [26]. In fact, Eq. (1) corresponds to Narayanaswamy’s original equation rewritten by Moynihan [15] who introduced the parameter  $x$ . An alternative relation[27] is offered by the generalization of the Adam-Gibbs expression, which connects, in equilibrium,  $\tau$  to the configurational entropy  $S_c$ . The resulting Adam-Gibbs-Scherer (AGS) expression is

$$\tau(T, T_f) = A' \exp \left[ \frac{E_A}{S_c(T_f)T} \right] \quad (2)$$

where

$$S_c(T) = \int_{T_K}^T \frac{\Delta C}{T} dT, \quad (3)$$

$T_K$  is the Kauzmann temperature,  $E_A$  is a constant, and  $\Delta C$  is the difference between the specific heats of the liquid and the glass. The TNM model requires  $\beta$  as a fitting parameter; additionally it requires the parameters ( $A$ ,  $x$ ,  $\Delta h^*$ ) for the Narayanaswamy-expression, or ( $A'$ ,  $E_A$ ,  $T_K$ ) for the AGS expression.

Figure 4 compares our MD results during the heating scan of the standard and hyperquenched glass with the predictions of the TNM model using both the Narayanaswamy and AGS expressions for  $\tau$ . A detailed analysis will be presented elsewhere[28]; here we show that both the Narayanaswamy and AGS expressions give satisfactory results only for the standard glass (Fig. 4(a)). The quality of the fit for the hyperquenched glass is unsatisfactory, as observed in the analysis of experimental data for hyperquenched samples[23], suggesting that in the hyperquenched experiments, the aging sample cannot be connected to a liquid at a fictive temperature  $T_f$ [29]. It also suggests that the application of the TNM approach for testing the shadow glass transition must be taken with caution[11].

In summary, we show by a proper numerical protocol that the complex phenomenology of the glass transition can be reproduced in simulations, notwithstanding the large differences in cooling rates. The TNM model which is able to describe the experimental specific heat for the standard cooling rate also describes the corresponding simulation results. One advantage of simulations is to shed light on phenomena that occur outside the experimentally-accessible region[30]. Our simulations show that the glass transition is characterized by a large specific heat peak, and when hyperquenched samples are annealed, the glass peak is anticipated at lower  $T$  by a pre-peak, with a much lower amplitude. This result

supports the recent reinterpretation of the existing experimental data [12], which identifies 136 K as the temperature of the pre-peak, and suggests  $\approx 165$  K as the ‘true’ glass transition temperature.

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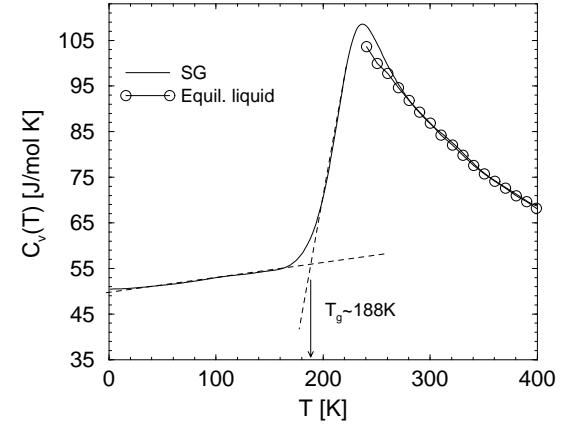


FIG. 1: Specific heat from MD simulations calculated by differentiating the total energy during heating of the standard glass (SG). Circles denote equilibrium values of  $C_V(T)$  in the liquid state.

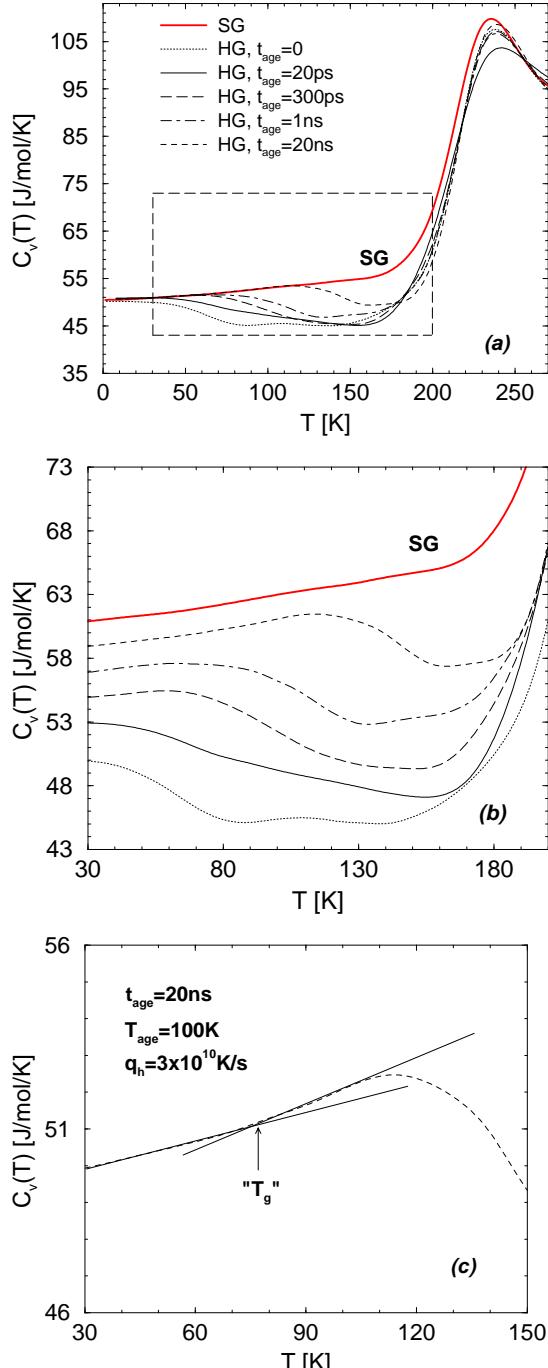


FIG. 2: (a)  $T$ -dependence of  $C_V$  for heating scans of the standard glass (SG) and the hyperquenched glass (HG). Also shown are the heating scans of the HG which has been annealed at  $T_{age} = 100$  K for four different aging times  $t_{age}$ . (b) Magnification of (a). Curves are shifted for clarity by 3 J/mol/K (for  $t_{age} = 20$  ps), 5 J/mol/K (for  $t_{age} = 300$  ps), 7 J/mol/K (for  $t_{age} = 1$  ns), 9 J/mol/K (for  $t_{age} = 20$  ns), and 11 J/mol/K (for SG). (c) Magnification of  $C_V(T)$  for the hyperquenched glass annealed at  $T_{age} = 100$  K for  $t_{age} = 20$  ns, to highlight the weak pre-peak at  $T \approx 113$  K. The straight lines show a possible construction that, in the absence of the peak at  $T \approx 220$  K, could be interpreted as the glass transition temperature " $T_g$ ".

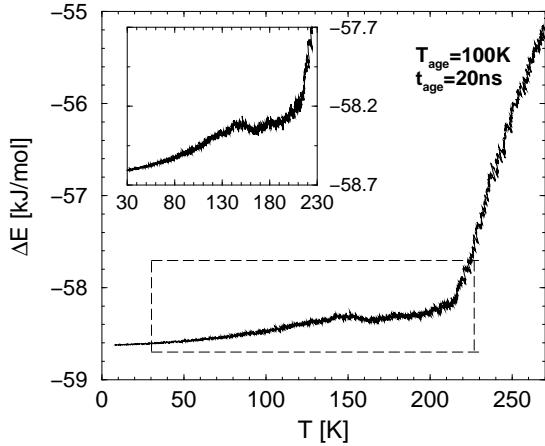


FIG. 3:  $T$  dependence of  $\Delta E \equiv E - 6RT$ , where  $E$  is the total energy per molecule,  $R$  is the gas constant, and  $6RT$  is the total energy of a glass of rigid molecules in the harmonic approximation, contributing a constant  $6R$  to  $C_V$ . Using  $\Delta E$  instead of  $E$  amplifies the very weak signal, whose derivative is responsible for the weak peak in  $C_V$  shown in Fig. 2(c).

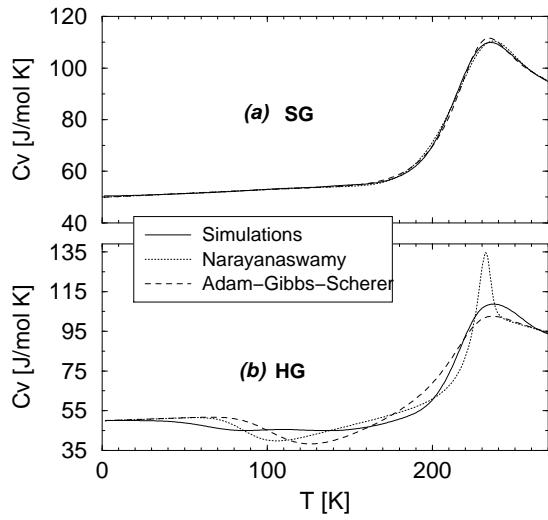


FIG. 4: Heating scans from the (a) standard glass (SG) and (b) hyperquenched glass (HG). Our simulations are compared with the predictions of the TNM model using both the Narayanaswamy model (fitting parameters for the SG are  $\ln(A/ns) = -22.36$ ,  $\beta = 0.525$ ,  $x = 0.635$ , and  $\Delta h^*/R = 4632$  K) and the Adam-Gibbs-Scherer expressions (fitting parameters for the SG are  $\ln(A/ns) = -9.86$ ,  $\beta = 0.519$ , and  $E_A = 27626$  kJ/mol; we use  $S_c$  from Ref. [32] and hence we do not require  $T_K$ ). We see that the TNM model describes the behavior of  $C_V(T)$  for the SG but fails for the HG.